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## 2D continuum viscodamage-embedded discontinuity model with second order mid-point scheme

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**Abstract.** This paper deals with numerical modeling of dynamic failure phenomena in rate-sensitive brittle and/or ductile materials. To this end, a two-dimensional continuum viscodamage-embedded discontinuity model, which is based on our previous work (see Do *et al.* 2017), is developed. More specifically, the pre-peak nonlinear and rate-sensitive hardening response of the material behavior, representing the fracture-process zone creation, is described by a rate-dependent continuum damage model. Meanwhile, an embedded displacement discontinuity model is used to formulate the post-peak response, involving the macro-crack creation accompanied by exponential softening. The numerical implementation in the context of the finite element method exploiting the second-order mid-point scheme is discussed in detail. In order to show the performance of the model several numerical examples are included.

**Keywords:** dynamics; fracture process zone-FPZ; strain-softening; localization; finite element; embedded discontinuity; mid-point scheme

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### 1. Introduction

According to Cervera *et al.* (1995): “As it is well known, brittle materials, especially concrete exhibit a rate-dependent behavior when subjected to high rate straining with significant increase of dynamic strengths and decrease of nonlinearity on the stress-strain response curves, when compared to those measured in static tests. Observational experience shows that rate sensitivity is primarily due to the fact that the growth of internal micro-cracking is retarded at high strain rate”. This characteristic of strong strain-rate sensitivity of brittle materials together with the presence of inertia effects cause principal modeling difficulties in the field of numerical simulation of crack propagation and localized failure analyses of structures and structural components under dynamic loading.

Starting from the observed evidence that this particular behavior is in fact consequence of the strain-rate dependency of the internal damage evolution, several rate-dependent continuum damage models were proposed concerning micro-crack interaction and growth under dynamic loading (e.g., Grady and Kipp 1980, Suaris and Shah 1984, Taylor *et al.* 1986, Fahrenthold 1991,

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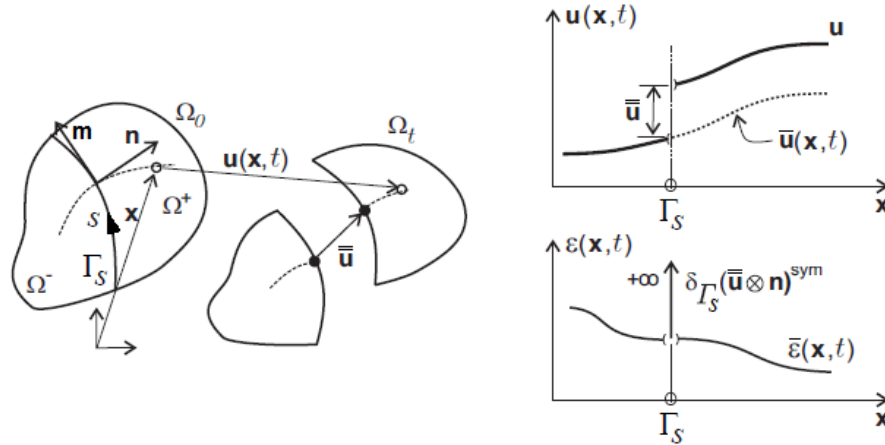


Fig. 1 The discontinuity surface  $\Gamma_S$  separating the domain  $\Omega$  into  $\Omega^+$  and  $\Omega^-$  and strong discontinuity kinematics

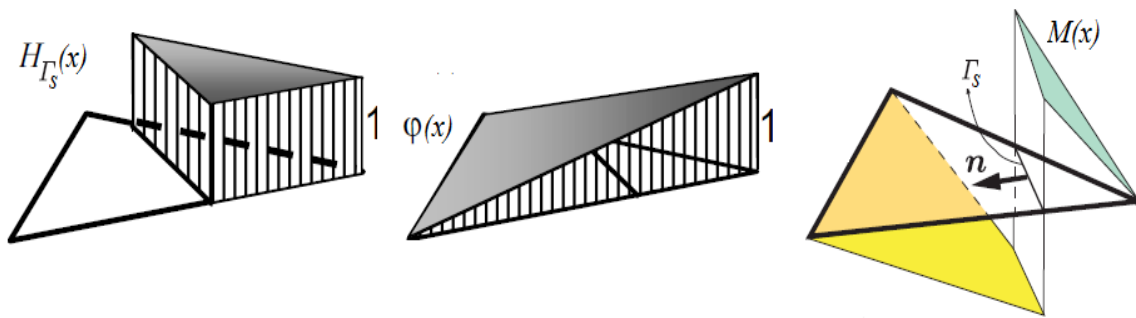


Fig. 2 Discontinuous shape function (2D case) for a CST element with constant discontinuity jumps

Yang *et al.* 1996, Yazdchi *et al.* 1996, Lu and Xu 2004, Wang *et al.* 2008, Hamdi *et al.* 2011). Even though the ill-posed problem due to strain softening, which is the source of major problems such as spurious mesh dependency, mesh alignment effects (De Borst *et al.* 1993) and failure without energy dissipation (Bažant 1976), can be avoided when rate-dependent constitutive relations are implemented carefully most of such continuum mechanics-based models, however, are not suitable to correctly predict damage localization processes where strain-softening phenomenon appears (see Bažant *et al.* 1984, Needleman 1988).

To avoid the problem outlined above the introduction of a localization limiter is required. One of the most promising relatively recent techniques for finite element modeling of crack propagation which can be employed for this purpose is the embedded strong discontinuity approach, in which the displacement field is enhanced to capture the discontinuity (crack) (e.g., Simo *et al.* 1993, Armero and Garikipati 1995, Oliver 1996, Oliver 2000, Alfaiate *et al.* 2002, Huespe *et al.* 2006, Ibrahimbegovic and Melnyk 2007, Linder and Armero 2007, Armero and Linder 2009, Brancherie and Ibrahimbegovic 2009, Radulovic *et al.* 2011, Dujc *et al.* 2013, Saksala *et al.* 2015), leading to a regularization of the modeling of reality. As the main novelty, herein we present a two-dimensional continuum viscodamage-embedded discontinuity model. This model concentrates on dynamic fracture, with an emphasis on crack phenomena, by using the mid-

point rule in order to carry out the time-integration for such a problem in each time step.

The outline of the paper is as follows: First, the theoretical formulation is briefly presented in Section 2. Next, Section 3 is devoted to numerical implementation where computational procedure is given in full detail, followed by Section 4 in which numerical simulations are performed and analyzed. Finally, some conclusions are drawn in Section 5.

## 2. Theoretical formulation

### 2.1 Rate-dependent continuum damage model

The internal energy of such a damage model can formally be written

$$\bar{\psi}(\bar{\boldsymbol{\varepsilon}}, \bar{\mathbf{D}}, \bar{\xi}) = \frac{1}{2} \bar{\boldsymbol{\varepsilon}} \cdot \bar{\mathbf{D}}^{-1} \bar{\boldsymbol{\varepsilon}} + \bar{\Xi}(\bar{\xi}) \quad (1)$$

where  $\bar{\xi}$  is the hardening variable, and  $\bar{\Xi}(\bar{\xi})$  stands for the corresponding hardening potential.

The damage function is defined by

$$\bar{\Phi}(\boldsymbol{\sigma}, \bar{q}) = \widehat{\Phi}(\boldsymbol{\sigma}) - (\bar{\sigma}_f - \bar{q}) \quad (2)$$

where  $\bar{\sigma}_f$  refers to the limit of elasticity indicating the first cracking and  $\bar{q}$  is a stress-like hardening variable which handles the damage threshold evolution.

By using the Legendre transformation to exchange the roles between the stress and deformation, we further introduce the complementary energy potential

$$\bar{\chi}(\boldsymbol{\sigma}, \bar{\mathbf{D}}, \bar{\xi}) = \boldsymbol{\sigma} \cdot \bar{\boldsymbol{\varepsilon}} - \bar{\psi}(\bar{\boldsymbol{\varepsilon}}, \bar{\mathbf{D}}, \bar{\xi}) = \frac{1}{2} \boldsymbol{\sigma} \cdot \bar{\mathbf{D}} \boldsymbol{\sigma} - \bar{\Xi}(\bar{\xi}) \quad (3)$$

By exploiting the second law of thermodynamics, we can obtain the explicit form of the damage model dissipation defined as follows

$$0 \leq \bar{\mathcal{D}} = \boldsymbol{\sigma} \cdot \dot{\bar{\boldsymbol{\varepsilon}}} - \dot{\bar{\psi}}(\bar{\boldsymbol{\varepsilon}}, \bar{\mathbf{D}}, \bar{\xi}) = \dot{\boldsymbol{\sigma}} \cdot (-\bar{\boldsymbol{\varepsilon}} + \bar{\mathbf{D}} \boldsymbol{\sigma}) + \frac{1}{2} \boldsymbol{\sigma} \cdot \dot{\bar{\mathbf{D}}} \boldsymbol{\sigma} - \frac{d\bar{\Xi}(\bar{\xi})}{d\bar{\xi}} \dot{\bar{\xi}} \quad (4)$$

In the case of “elastic” process where  $\dot{\bar{\mathbf{D}}} = 0$  and  $\dot{\bar{\xi}} = 0$ , the dissipation inequality (the Clausius-Duhem inequality) above becomes an equality with  $\bar{\mathcal{D}} = 0$ . This leads to the appropriate form of constitutive equations for damage model

$$\dot{\boldsymbol{\sigma}} \cdot (-\bar{\boldsymbol{\varepsilon}} + \bar{\mathbf{D}} \boldsymbol{\sigma}) = 0 \Leftrightarrow \bar{\boldsymbol{\varepsilon}} = \bar{\mathbf{D}} \boldsymbol{\sigma} \Rightarrow \boldsymbol{\sigma} = \bar{\mathbf{D}}^{-1} \bar{\boldsymbol{\varepsilon}} = \frac{\partial \bar{\psi}(\bar{\boldsymbol{\varepsilon}}, \bar{\mathbf{D}}, \bar{\xi})}{\partial \bar{\boldsymbol{\varepsilon}}}; \bar{q} = -\frac{d\bar{\Xi}(\bar{\xi})}{d\bar{\xi}} \quad (5)$$

By assuming that these equations remain valid for an inelastic process with  $\dot{\bar{\mathbf{D}}} \neq 0$ ;  $\dot{\bar{\xi}} \neq 0$ , we can redefine the damage dissipation

$$0 < \bar{\mathcal{D}} = \frac{1}{2} \boldsymbol{\sigma} \cdot \dot{\bar{\mathbf{D}}} \boldsymbol{\sigma} - \frac{d\bar{\Xi}(\bar{\xi})}{d\bar{\xi}} \dot{\bar{\xi}} = \frac{1}{2} \boldsymbol{\sigma} \cdot \dot{\bar{\mathbf{D}}} \boldsymbol{\sigma} + \bar{q} \dot{\bar{\xi}} \quad (6)$$

Here in order to seek the best formulation for high-order scheme such as the mid-point, we introduce the main novelty of using the viscous regularization of damage, leading to visco-damage. This is obtained by using the regularized maximum dissipation to enforce the constraint  $\bar{\Phi}(\boldsymbol{\sigma}, \bar{q}) \leq 0$ . Such form of the damage model is capable of taking into account rate-sensitivity of the response and it is further referred as visco-damage. To that end, the problem can be recast as the unconstrained maximization problem

$$\max_{\bar{\Phi}(\boldsymbol{\sigma}, \bar{q}) \leq 0} [\bar{\mathcal{D}}(\boldsymbol{\sigma}, \bar{q})] \Leftrightarrow \max_{\dot{\gamma} \geq 0} \min_{\forall(\boldsymbol{\sigma}, \bar{q})} \underbrace{[-\bar{\mathcal{D}}(\boldsymbol{\sigma}, \bar{\mathbf{D}}, \bar{\xi}) + \bar{P}(\bar{\Phi}(\boldsymbol{\sigma}, \bar{q}))]}_{\bar{\mathcal{L}}(\boldsymbol{\sigma}, \bar{\mathbf{D}}, \bar{\xi}, \bar{q})} \quad (7)$$

where  $\bar{P}(\bar{\Phi}(\boldsymbol{\sigma}, \bar{q}))$ , a quadratic form of the penalty term, is defined by

$$\bar{P}(\bar{\Phi}(\boldsymbol{\sigma}, \bar{q})) = \begin{cases} \frac{1}{2\bar{\eta}} \bar{\Phi}^2; & \bar{\Phi} > 0 \\ 0; & \bar{\Phi} \leq 0 \end{cases} \quad (8)$$

where  $\bar{\eta}$  is the viscosity parameter for continuum damage model.

By applying the Kuhn-Tucker optimality conditions for the chosen damage Lagrangian the evolution equations for the internal variables can thus be written

$$\begin{aligned} 0 &= \frac{\partial \bar{\mathcal{L}}(\boldsymbol{\sigma}, \bar{\mathbf{D}}, \bar{\xi}, \bar{q})}{\partial \boldsymbol{\sigma}} = -\dot{\bar{\mathbf{D}}} \boldsymbol{\sigma} + \frac{\langle \bar{\Phi} \rangle}{\bar{\eta}} \frac{\partial \bar{\Phi}(\boldsymbol{\sigma}, \bar{q})}{\partial \boldsymbol{\sigma}} \\ 0 &= \frac{\partial \bar{\mathcal{L}}(\boldsymbol{\sigma}, \bar{\mathbf{D}}, \bar{\xi}, \bar{q})}{\partial \bar{q}} = -\dot{\bar{\xi}} + \frac{\langle \bar{\Phi} \rangle}{\bar{\eta}} \frac{\partial \bar{\Phi}(\boldsymbol{\sigma}, \bar{q})}{\partial \bar{q}} \end{aligned} \quad (9)$$

where symbol  $\langle \cdot \rangle$  denotes the Macauley parenthesis, which will filter out only the positive value of its argument.

For  $\widehat{\Phi}(\boldsymbol{\sigma})$ , a homogeneous function of degree one, implies that  $\frac{\partial \bar{\Phi}}{\partial \boldsymbol{\sigma}} \boldsymbol{\sigma} = \widehat{\Phi}(\boldsymbol{\sigma})$ , we can rewrite (9)<sub>1</sub> as

$$\dot{\bar{\mathbf{D}}} = \frac{\langle \bar{\Phi} \rangle}{\bar{\eta}} \frac{1}{\widehat{\Phi}(\boldsymbol{\sigma})} \frac{\partial \bar{\Phi}}{\partial \boldsymbol{\sigma}} \otimes \frac{\partial \bar{\Phi}}{\partial \boldsymbol{\sigma}} \quad (10)$$

By introducing the new definition of damage multiplier  $\dot{\gamma} = \frac{\langle \bar{\Phi} \rangle}{\bar{\eta}}$ , the evolution equation for rate-sensitive damage model in (9) can be recast in standard format as

$$\begin{aligned} \dot{\bar{\mathbf{D}}} &= \dot{\gamma} \frac{1}{\widehat{\Phi}(\boldsymbol{\sigma})} \frac{\partial \bar{\Phi}}{\partial \boldsymbol{\sigma}} \otimes \frac{\partial \bar{\Phi}}{\partial \boldsymbol{\sigma}} \\ \dot{\bar{\xi}} &= \dot{\gamma} \frac{\partial \bar{\Phi}}{\partial \bar{q}} \end{aligned} \quad (11)$$

We note that the damage multiplier can be directly computed from the current (positive) value of damage function. From there, for the isotropic case, damage model is characterized by

$$\begin{aligned}\bar{\Phi}(\boldsymbol{\sigma}, \bar{q}) &= \frac{\sqrt{\boldsymbol{\sigma} \cdot \mathbf{D}^e \boldsymbol{\sigma}}}{\|\boldsymbol{\sigma}\|_{\mathbf{D}^e}} - \frac{1}{\sqrt{E}} (\bar{\sigma}_f - \bar{q}); \quad \dot{\gamma} = \frac{\langle \dot{\bar{\Phi}}(\boldsymbol{\sigma}, \bar{q}) \rangle}{\bar{\eta}} \\ \dot{\bar{\mathbf{D}}} &= \dot{\gamma} \frac{\mathbf{D}^e}{\|\boldsymbol{\sigma}\|_{\mathbf{D}^e}} = \dot{\mu} \mathbf{D}^e; \quad \dot{\xi} = \dot{\gamma} \frac{1}{\sqrt{E}}; \quad \dot{\mu} = \frac{\dot{\gamma}}{\|\boldsymbol{\sigma}\|_{\mathbf{D}^e}} \\ \bar{\mathbf{D}} &= (1 + \bar{\mu}) \mathbf{D}^e = (1 + \bar{\mu}) \mathbf{C}^{e-1}\end{aligned}\quad (12)$$

where  $\mathbf{D}^e$  denotes the undamaged elastic compliance tensor of the bulk material, which is equal to the inverse of elasticity tensor,  $\mathbf{D}^e = [\mathbf{C}^e]^{-1}$ , and  $E$  refers to the Young's modulus.

We can further simplify the stress computation for the isotropic damage model of kind to

$$\boldsymbol{\sigma} = \mathbf{C}^e (1 - d) \bar{\boldsymbol{\epsilon}}; \quad d = \frac{\bar{\mu}}{1 + \bar{\mu}}; \quad d \in [0, 1] \quad (13)$$

## 2.2 Discrete damage model

Once the peak resistance is reached, the softening phase will start. Here, the crack leads to the total displacement field that can be written as the sum of a continuous regular part  $\bar{\mathbf{u}}(\mathbf{x}, t)$  and a discontinuous irregular part corresponding to the displacement jump  $\bar{\bar{\mathbf{u}}}(\mathbf{x}, t)$  (see Fig. 1)

$$\mathbf{u}(\mathbf{x}, t) = \bar{\mathbf{u}}(\mathbf{x}, t) + \bar{\bar{\mathbf{u}}}(\mathbf{x}, t) H_{\Gamma_s}(\mathbf{x}) \quad (14)$$

where  $H_{\Gamma_s}(\mathbf{x})$  denotes the Heaviside function (see Fig. 2)

$$H_{\Gamma_s}(\mathbf{x}) = \begin{cases} 1 & \mathbf{x} \in \partial\Omega^- \\ 0 & \mathbf{x} \in \partial\Omega^+ \end{cases} \quad (15)$$

with  $\partial\Omega^-$  and  $\partial\Omega^+$  are the boundary of two sub-domains of the element separated by the discontinuity  $\Gamma_s$ .

$$\partial\Omega^- = \partial\Omega \cap \Omega^- \quad \partial\Omega^+ = \partial\Omega \cap \Omega^+ \quad (16)$$

and  $\Gamma_s$  is the discontinuity surface separating the continuous domain  $\Omega$  into two sub-domains  $\Omega^+$  and  $\Omega^-$ .

The infinitesimal strain which corresponds to this displacement decomposition can be then computed as

$$\boldsymbol{\varepsilon}(\mathbf{x}, t) = \nabla^s \mathbf{u}(\mathbf{x}, t) = \nabla^s \bar{\mathbf{u}}(\mathbf{x}, t) + H_{\Gamma_s} \nabla^s \bar{\bar{\mathbf{u}}}(\mathbf{x}, t) + \left( \bar{\bar{\mathbf{u}}}(\mathbf{x}, t) \nabla H_{\Gamma_s}(\mathbf{x}) \right)^s \quad (17)$$

where superscript  $[\bullet]^s$  stands for the symmetric part of  $[\bullet]$ .

We also note that  $[\bullet \nabla H_{\Gamma_s}(\mathbf{x})]^s = \delta_{\Gamma_s}(\mathbf{x})(\bullet \otimes \mathbf{n})^s$ , where  $\otimes$  denotes a dyadic product,  $\delta_{\Gamma_s}(\mathbf{x})$  is the Dirac-delta function along surface  $\Gamma_s$  and  $\mathbf{n}$  is the unit normal vector, then

$$\boldsymbol{\varepsilon}(\mathbf{x}, t) = \nabla^s \mathbf{u}(\mathbf{x}, t) = \nabla^s \bar{\mathbf{u}}(\mathbf{x}, t) + H_{\Gamma_s} \nabla^s \bar{\bar{\mathbf{u}}}(\mathbf{x}, t) + \delta_{\Gamma_s}(\mathbf{x})(\bar{\bar{\mathbf{u}}}(\mathbf{x}, t) \otimes \mathbf{n})^s \quad (18)$$

Eq. (18) states that the infinitesimal strain at localization can be divided into a regular (continuous) part,  $\bar{\boldsymbol{\varepsilon}}(\mathbf{x}, t)$ , and a singular (discontinuous) part,  $\bar{\bar{\boldsymbol{\varepsilon}}}(\mathbf{x}, t)$ , according to

$$\boldsymbol{\varepsilon}(\mathbf{x}, t) = \bar{\boldsymbol{\varepsilon}}(\mathbf{x}, t) + \bar{\bar{\boldsymbol{\varepsilon}}}(\mathbf{x}, t) \delta_{\Gamma_s}(\mathbf{x}) \quad (19)$$

in which

$$\bar{\boldsymbol{\varepsilon}}(\mathbf{x}, t) = \nabla^s \bar{\mathbf{u}}(\mathbf{x}, t) + H_{\Gamma_s} \nabla^s \bar{\bar{\mathbf{u}}}(\mathbf{x}, t) = \nabla^s \bar{\mathbf{u}}(\mathbf{x}, t) \quad (20)$$

and

$$\bar{\bar{\boldsymbol{\varepsilon}}}(\mathbf{x}, t) = (\bar{\bar{\mathbf{u}}}(\mathbf{x}, t) \otimes \mathbf{n})^s \quad (21)$$

By taking into account that the stress field in Eq. (5) remains bounded, we can conclude that the damage compliance tensor  $\mathbf{D}$  should also be split into two parts: regular and singular

$$\mathbf{D} = \bar{\mathbf{D}} + \bar{\bar{\mathbf{D}}} \delta_{\Gamma_s} \quad (22)$$

By comparing this against (20) and (21), we can identify

$$\begin{cases} \nabla^s \bar{\mathbf{u}}(\mathbf{x}, t) = \bar{\mathbf{D}} \boldsymbol{\sigma} & \text{on } \Omega \setminus \Gamma_s \\ (\bar{\bar{\mathbf{u}}}(\mathbf{x}, t) \otimes \mathbf{n})^s = \bar{\bar{\mathbf{D}}} \boldsymbol{\sigma} & \text{on } \Gamma_s \end{cases} \quad (23)$$

The decomposition of the strain field into a regular part and singular part leads to the corresponding split of hardening variable  $\xi = \bar{\xi} + \bar{\bar{\xi}} \delta_{\Gamma_s}$ . With these results in hand, we can finally write the Helmholtz free energy split into a regular part  $\bar{\psi}$  from fracture process zone on  $\Omega \setminus \Gamma_s$  and a singular part  $\bar{\bar{\psi}}$  associated to the discontinuity on  $\Gamma_s$

$$\psi(\boldsymbol{\varepsilon}, \mathbf{D}, \xi) = \underbrace{\frac{1}{2} \bar{\boldsymbol{\varepsilon}} \cdot \bar{\mathbf{D}}^{-1} \bar{\boldsymbol{\varepsilon}} + \bar{\Xi}(\bar{\xi})}_{\bar{\psi}(\bar{\boldsymbol{\varepsilon}}, \bar{\mathbf{D}}, \bar{\xi})} + \underbrace{\left[ \frac{1}{2} \bar{\mathbf{u}} \cdot \bar{\mathbf{Q}}^{-1} \bar{\mathbf{u}} + \bar{\Xi}(\bar{\xi}) \right]}_{\bar{\psi}(\bar{\mathbf{u}}, \bar{\mathbf{Q}}, \bar{\xi})} \delta_{\Gamma_s} \quad (24)$$

where  $\bar{\mathbf{Q}} = (\mathbf{n} \cdot \bar{\mathbf{D}} \mathbf{n})^{-1}$  and  $\bar{\Xi}(\bar{\xi})$  is the softening potential that measures the fracture energy of a particular material.

The total dissipation of the material can then be expressed as the sum of the bulk dissipation due to diffuse damage mechanisms and the localized dissipation due to the development of localization zones

$$0 \leq \mathcal{D} = \bar{\mathcal{D}} + \bar{\mathcal{D}} \delta_{\Gamma_s} = \boldsymbol{\sigma} \cdot \dot{\boldsymbol{\varepsilon}} - \frac{d}{dt} \bar{\psi}(\bar{\boldsymbol{\varepsilon}}, \bar{\mathbf{D}}, \bar{\xi}) + \left[ \mathbf{t}_{\Gamma_s} \cdot \dot{\bar{\mathbf{u}}} - \frac{d}{dt} \bar{\psi}(\bar{\mathbf{u}}, \bar{\mathbf{Q}}, \bar{\xi}) \right] \delta_{\Gamma_s} \quad (25)$$

where the second term is the singular part of dissipation, which can be written

$$\begin{aligned} 0 \leq \bar{\mathcal{D}} &= \mathbf{t}_{\Gamma_s} \cdot \dot{\bar{\mathbf{u}}} - \frac{\partial \bar{\psi}}{\partial \bar{\mathbf{u}}} \cdot \frac{\partial \bar{\mathbf{u}}}{\partial t} - \frac{\partial \bar{\psi}}{\partial \bar{\mathbf{Q}}} \cdot \frac{\partial \bar{\mathbf{Q}}}{\partial t} - \frac{\partial \bar{\psi}}{\partial \bar{\xi}} \frac{\partial \bar{\xi}}{\partial t} \\ &= (\mathbf{t}_{\Gamma_s} - \bar{\mathbf{Q}}^{-1} \bar{\mathbf{u}}) \dot{\bar{\mathbf{u}}} + \frac{1}{2} \mathbf{t}_{\Gamma_s} \cdot \dot{\bar{\mathbf{Q}}} \mathbf{t}_{\Gamma_s} - \frac{d \bar{\Xi}(\bar{\xi})}{d \bar{\xi}} \dot{\bar{\xi}} \end{aligned} \quad (26)$$

Each damage dissipation mechanism activation is controlled by the corresponding damage criterion. For the surface of discontinuity, we assume the damage function as

$$\bar{\Phi}(\mathbf{t}_{\Gamma_s}, \bar{q}) = \hat{\hat{\Phi}}(\mathbf{t}_{\Gamma_s}) - (\bar{\sigma}_f - \bar{q}) \quad (27)$$

where  $\mathbf{t}_{\Gamma_s} = (\boldsymbol{\sigma} \mathbf{n})|_{\Gamma_s}$  is the traction vector acting on discontinuity,  $\hat{\hat{\Phi}}(\mathbf{t}_{\Gamma_s})$  is a homogeneous function of degree one, i.e.,  $\frac{\partial \bar{\Phi}}{\partial \mathbf{t}_{\Gamma_s}} \mathbf{t}_{\Gamma_s} = \frac{\partial \hat{\hat{\Phi}}}{\partial \mathbf{t}_{\Gamma_s}} \mathbf{t}_{\Gamma_s} = \hat{\hat{\Phi}}(\mathbf{t}_{\Gamma_s})$ ,  $\bar{\sigma}_f$  is the initial damage threshold and  $\bar{q}$  is the softening traction-like variable controlling the evolution of the damage threshold.

In an elastic process, with no change of internal variables and zero dissipation ( $\dot{\bar{\mathbf{Q}}} = 0, \dot{\bar{\xi}} = 0, \bar{\mathcal{D}} = 0$ ), Eq. (26) allows us to define the form of constitutive equation and the traction-like variable associated to softening phenomena at the discontinuity

$$(\mathbf{t}_{\Gamma_s} - \bar{\mathbf{Q}}^{-1} \bar{\mathbf{u}}) \dot{\bar{\mathbf{u}}} = 0 \Leftrightarrow \mathbf{t}_{\Gamma_s} = \bar{\mathbf{Q}}^{-1} \bar{\mathbf{u}} = \frac{\partial \bar{\psi}(\bar{\mathbf{u}}, \bar{\mathbf{Q}}, \bar{\xi})}{\partial \bar{\mathbf{u}}}; \bar{q} = -\frac{d \bar{\Xi}(\bar{\xi})}{d \bar{\xi}} \quad (28)$$

By assuming that these relations also hold in damage process, from Eq. (26) we can obtain a reduced form of the inelastic localized dissipation as

$$0 < \bar{\mathcal{D}} = \frac{1}{2} \mathbf{t}_{\Gamma_s} \cdot \dot{\bar{\mathbf{Q}}} \mathbf{t}_{\Gamma_s} - \frac{d \bar{\Xi}(\bar{\xi})}{d \bar{\xi}} \dot{\bar{\xi}} = \frac{1}{2} \mathbf{t}_{\Gamma_s} \cdot \dot{\bar{\mathbf{Q}}} \mathbf{t}_{\Gamma_s} + \bar{q} \dot{\bar{\xi}} \quad (29)$$



Using the principle of maximum of damage dissipation we can choose the traction which will maximize the damage dissipation among all admissible candidates in the sense of the chosen damage criterion. Similar to continuum damage model, we also choose an alternative form of the discrete damage model, which is capable of taking into account rate-sensitivity of the response, resulting in

$$\max_{\bar{\Phi}(\mathbf{t}_{\Gamma_s}, \bar{q}) \leq 0} [\bar{D}(\mathbf{t}_{\Gamma_s}, \bar{q})] \Leftrightarrow \max_{\dot{\bar{\gamma}} \geq 0} \min_{\forall(\mathbf{t}_{\Gamma_s}, \bar{q})} \underbrace{[-\bar{D}(\mathbf{t}_{\Gamma_s}, \bar{\mathbf{Q}}, \bar{\xi}) + \bar{P}(\bar{\Phi}(\mathbf{t}_{\Gamma_s}, \bar{q}))]}_{\bar{\mathcal{L}}(\mathbf{t}_{\Gamma_s}, \bar{\mathbf{Q}}, \bar{\xi}, \bar{q})} \tag{30}$$

where  $\bar{P}(\bar{\Phi}(\mathbf{t}_{\Gamma_s}, \bar{q}))$  stands for a quadratic form of the penalty term for discontinuity.

$$\bar{P}(\bar{\Phi}(\mathbf{t}_{\Gamma_s}, \bar{q})) = \begin{cases} \frac{1}{2\bar{\eta}} \bar{\Phi}^2; & \bar{\Phi} > 0 \\ 0; & \bar{\Phi} \leq 0 \end{cases} \tag{31}$$

The internal variables can be obtained by using the corresponding Kuhn-Tucker optimality conditions, according to

$$\begin{aligned} 0 &= \frac{\partial \bar{\mathcal{L}}(\mathbf{t}_{\Gamma_s}, \bar{\mathbf{Q}}, \bar{\xi}, \bar{q})}{\partial \mathbf{t}_{\Gamma_s}} = -\dot{\bar{\mathbf{Q}}}\mathbf{t}_{\Gamma_s} + \frac{\langle \bar{\Phi} \rangle}{\bar{\eta}} \frac{\partial \bar{\Phi}(\mathbf{t}_{\Gamma_s}, \bar{q})}{\partial \mathbf{t}_{\Gamma_s}} \\ 0 &= \frac{\partial \bar{\mathcal{L}}(\mathbf{t}_{\Gamma_s}, \bar{\mathbf{Q}}, \bar{\xi}, \bar{q})}{\partial \bar{q}} = -\dot{\bar{\xi}} + \frac{\langle \bar{\Phi} \rangle}{\bar{\eta}} \frac{\partial \bar{\Phi}(\mathbf{t}_{\Gamma_s}, \bar{q})}{\partial \bar{q}} \end{aligned} \tag{32}$$

By introducing the softening damage multiplier  $\dot{\bar{\gamma}} = \frac{\langle \bar{\Phi} \rangle}{\bar{\eta}}$ , Eq. (32) can be rewritten as

$$\begin{aligned} \dot{\bar{\mathbf{Q}}} &= \dot{\bar{\gamma}} \frac{1}{\bar{\Phi}(\mathbf{t}_{\Gamma_s})} \frac{\partial \bar{\Phi}}{\partial \mathbf{t}_{\Gamma_s}} \otimes \frac{\partial \bar{\Phi}}{\partial \mathbf{t}_{\Gamma_s}} \\ \dot{\bar{\xi}} &= \dot{\bar{\gamma}} \frac{\partial \bar{\Phi}}{\partial \mathbf{t}_{\Gamma_s}} \end{aligned} \tag{33}$$

For a 2D anisotropic damage model (two-surface damage model), considering the principle of maximum damage dissipation under the two constraints:  $\bar{\Phi}_1 \leq 0$  and  $\bar{\Phi}_2 \leq 0$  and exploiting Kuhn-Tucker optimality conditions allow us to obtain the following evolution equations for internal variables

$$\begin{aligned} \max_{\bar{\Phi}_1 \leq 0, \bar{\Phi}_2 \leq 0} [\bar{D}(\mathbf{t}_{\Gamma_s}, \bar{q})] &\Leftrightarrow \max_{\dot{\bar{\gamma}}_1 \geq 0, \dot{\bar{\gamma}}_2 \geq 0} \min_{\forall(\mathbf{t}_{\Gamma_s}, \bar{q})} \underbrace{[-\bar{D}(\mathbf{t}_{\Gamma_s}, \bar{\mathbf{Q}}, \bar{\xi}) + \bar{P}_1(\bar{\Phi}_1(\mathbf{t}_{\Gamma_s}, \bar{q})) + \bar{P}_2(\bar{\Phi}_2(\mathbf{t}_{\Gamma_s}, \bar{q}))]}_{\bar{\mathcal{L}}(\mathbf{t}_{\Gamma_s}, \bar{\mathbf{Q}}, \bar{\xi}, \bar{q})} \\ \frac{\partial \bar{\mathcal{L}}}{\partial \mathbf{t}_{\Gamma_s}} &= -\dot{\bar{\mathbf{Q}}}\mathbf{t}_{\Gamma_s} + \frac{\partial \bar{P}_1}{\partial \mathbf{t}_{\Gamma_s}} + \frac{\partial \bar{P}_2}{\partial \mathbf{t}_{\Gamma_s}} = 0 \Rightarrow \dot{\bar{\mathbf{Q}}} = \frac{\langle \bar{\Phi}_1 \rangle}{\bar{\eta}_1} \frac{1}{\mathbf{n} \cdot \mathbf{t}_{\Gamma_s}} \mathbf{n} \otimes \mathbf{n} + \frac{\langle \bar{\Phi}_2 \rangle}{\bar{\eta}_2} \frac{1}{|\mathbf{m} \cdot \mathbf{t}_{\Gamma_s}|} \mathbf{m} \otimes \mathbf{m} \\ \frac{\partial \bar{\mathcal{L}}}{\partial \bar{q}} &= -\dot{\bar{\xi}} + \frac{\partial \bar{P}_1}{\partial \bar{q}} + \frac{\partial \bar{P}_2}{\partial \bar{q}} = 0 \Rightarrow \dot{\bar{\xi}} = \frac{\langle \bar{\Phi}_1 \rangle}{\bar{\eta}_1} \frac{\partial \bar{\Phi}_1}{\partial \bar{q}} + \frac{\langle \bar{\Phi}_2 \rangle}{\bar{\eta}_2} \frac{\partial \bar{\Phi}_2}{\partial \bar{q}} = \frac{\langle \bar{\Phi}_1 \rangle}{\bar{\eta}_1} + \frac{\langle \bar{\Phi}_2 \rangle}{\bar{\eta}_2} \frac{\bar{\sigma}_s}{\bar{\sigma}_f} \end{aligned} \tag{34}$$

### 3. Numerical implementation – Finite element with embedded strong discontinuities

#### 3.2 Enhanced kinematics

As aforementioned, once the failure in a local zone occurs, the enhanced displacement field ought to be introduced and written as the sum of a regular part and an irregular part (see Fig. 1). In this direction, we present herein the finite element interpolations for a triangular three-node element (CST) in which the displacement jump is taken into account as constant.

Deriving from feature of the continuous regular part  $\bar{\mathbf{u}}(\mathbf{x}, t)$  which can be written as

$$\bar{\mathbf{u}}(\mathbf{x}, t) = \hat{\mathbf{u}}(\mathbf{x}, t) - \bar{\bar{\mathbf{u}}}(\mathbf{x}, t)\varphi(\mathbf{x}) \quad (35)$$

Eq. (14) can further be written

$$\mathbf{u}(\mathbf{x}, t) = \hat{\mathbf{u}}(\mathbf{x}, t) + \bar{\bar{\mathbf{u}}}(\mathbf{x}, t)[H_{\Gamma_s}(\mathbf{x}) - \varphi(\mathbf{x})] \quad (36)$$

where  $\varphi(\mathbf{x})$  is the smooth function and  $\hat{\mathbf{u}}(\mathbf{x}, t)$  is the classic displacement interpolation of a CST element from which we can get the standard strain field

$$\hat{\mathbf{u}}(\mathbf{x}, t) = \sum_{a=1}^3 \mathbf{N}_a(\mathbf{x})\mathbf{u}_a = \mathbf{N}\mathbf{d} \Rightarrow \hat{\boldsymbol{\varepsilon}}(\mathbf{x}, t) = \sum_{a=1}^3 \frac{\mathbf{L}\mathbf{N}_a(\mathbf{x})}{\mathbf{B}_a(\mathbf{x})}\mathbf{u}_a = \mathbf{B}\mathbf{d} \quad (37)$$

in which  $\mathbf{u}_a$  refers to the displacement of node  $a$ ,  $\mathbf{N}_a(\mathbf{x})$  stands for the shape function associated to node  $a$  and  $\mathbf{L}$  denotes the matrix form of the strain-displacement operator  $\nabla^s$ .

By introducing an additional shape function  $\mathbf{M}(\mathbf{x}) = H_{\Gamma_s}(\mathbf{x}) - \varphi(\mathbf{x})$  shown in Fig. 2, the following approximation combining Eqs. (36) and (37) is considered for the enhanced displacement field

$$\mathbf{u}(\mathbf{x}, t) = \sum_{a=1}^3 \mathbf{N}_a(\mathbf{x})\mathbf{u}_a + \mathbf{M}(\mathbf{x})\bar{\bar{\mathbf{u}}}(\mathbf{x}, t) = \mathbf{N}\mathbf{d} + \mathbf{M}\bar{\bar{\mathbf{u}}} \quad (38)$$

The real strain field interpolation remains similar to the interpolation of virtual strain field

$$\boldsymbol{\varepsilon}(\mathbf{x}, t) = \mathbf{B}\mathbf{d} + \mathbf{G}_r\bar{\bar{\mathbf{u}}} \Rightarrow \delta\boldsymbol{\varepsilon}(\mathbf{x}, t) = \mathbf{B}\mathbf{w} + \mathbf{G}_v\bar{\bar{\boldsymbol{\beta}}} \quad (39)$$

where  $\mathbf{B}_a(\mathbf{x}) = \mathbf{L}\mathbf{N}_a(\mathbf{x})$ ,  $\mathbf{G}_r(\mathbf{x}) = \mathbf{L}\mathbf{M}(\mathbf{x})$ ,  $\mathbf{w}$  and  $\bar{\bar{\boldsymbol{\beta}}}$  represent the virtual displacement and virtual displacement jump fields, respectively.  $\mathbf{G}_v(\mathbf{x})$  is referred to as an incompatible mode function modified in order to satisfy the patch-test condition. In concordance with the form of the function  $\mathbf{M}(\mathbf{x})$ ,  $\mathbf{G}_r(\mathbf{x})$  and  $\mathbf{G}_v(\mathbf{x})$  must be decomposed into a regular part and a singular part as

$$\mathbf{G}_r(\mathbf{x}) = \bar{\bar{\mathbf{G}}}_r(\mathbf{x}) + \bar{\bar{\mathbf{G}}}_r(\mathbf{x})\delta_{\Gamma_s} \quad \mathbf{G}_v(\mathbf{x}) = \mathbf{G}_r(\mathbf{x}) - \frac{1}{A^e} \int_{\Omega^e} \mathbf{G}_r(\mathbf{x})d\Omega^e = \bar{\bar{\mathbf{G}}}_v + \bar{\bar{\mathbf{G}}}_v\delta_{\Gamma_s} \quad (40)$$

#### 3.2 Computational procedure

The operator split solution procedure is used for the solution of the problem. The local computation is started by assuming the elastic trial step with no evolution of internal variables at time step  $t_{n+\frac{1}{2}}$ , namely

$$\bar{\gamma}_{n+\frac{1}{2}} = 0, \bar{\xi}_{n+\frac{1}{2}}^{trial} = \bar{\xi}_n, \bar{\mathbf{D}}_{n+\frac{1}{2}}^{trial} = \bar{\mathbf{D}}_n, \bar{q}_{n+\frac{1}{2}}^{trial} = \bar{q}_n, \boldsymbol{\sigma}_{n+\frac{1}{2}}^{trial} = \bar{\mathbf{D}}_n^{-1} \bar{\boldsymbol{\epsilon}}_{n+\frac{1}{2}} \quad (41)$$

We can thus readily compute the trial values of damage function

$$\bar{\Phi}_{n+\frac{1}{2}}^{trial} = \left\| \boldsymbol{\sigma}_{n+\frac{1}{2}}^{trial} \right\|_{\mathbf{D}^e} - \frac{1}{\sqrt{E}} (\bar{\sigma}_f - \bar{q}_n) \quad (42)$$

If  $\bar{\Phi}_{n+\frac{1}{2}}^{trial} \leq 0$ , the trial state is admissible. In the opposite case where  $\bar{\Phi}_{n+\frac{1}{2}}^{trial} > 0$ , evolution of internal variables should be computed, according to

$$\begin{aligned} \bar{\mathbf{D}}_{n+\frac{1}{2}} &= \left( 1 + \bar{\mu}_{n+\frac{1}{2}} \right) \mathbf{D}^e \\ \bar{\xi}_{n+1} - \bar{\xi}_n &= \bar{\gamma}_{n+\frac{1}{2}} \frac{1}{\sqrt{E}} \\ \bar{\xi}_{n+\frac{1}{2}} &= \frac{\bar{\xi}_{n+1} + \bar{\xi}_n}{2} \\ \bar{q}_{n+\frac{1}{2}} &= \frac{\bar{q}_{n+1} + \bar{q}_n}{2} \end{aligned} \quad (43)$$

Exploiting equation  $\dot{\bar{\gamma}}_{n+\frac{1}{2}} = \frac{\bar{\gamma}_{n+\frac{1}{2}}}{\Delta t} = \frac{\langle \bar{\Phi}_{n+\frac{1}{2}} \rangle}{\bar{\eta}}$ , the Lagrange multiplier  $\bar{\gamma}_{n+\frac{1}{2}}$  can be computed as follows

$$\bar{\gamma}_{n+\frac{1}{2}} = \frac{\bar{\Phi}_{n+\frac{1}{2}}^{trial}}{\frac{\bar{\eta}}{\Delta t} + \frac{1}{2(1+\bar{\mu}_n)} + \frac{K}{2E}} \quad (44)$$

which allows us to deduce the following expressions

$$\begin{aligned} \bar{\mu}_{n+1} &= \bar{\mu}_n + \frac{\bar{\gamma}_{n+\frac{1}{2}}}{\left\| \boldsymbol{\sigma}_{n+\frac{1}{2}} \right\|_{\mathbf{D}^e}} = \bar{\mu}_n + \frac{\bar{\gamma}_{n+\frac{1}{2}}}{\left\| \boldsymbol{\sigma}_{n+\frac{1}{2}}^{trial} \right\|_{\mathbf{D}^e} - \frac{\bar{\gamma}_{n+\frac{1}{2}}}{2(1+\bar{\mu}_n)}} \\ \bar{\mu}_{n+\frac{1}{2}} &= \frac{\bar{\mu}_{n+1} + \bar{\mu}_n}{2} \\ \boldsymbol{\sigma}_{n+\frac{1}{2}} &= \boldsymbol{\sigma}_{n+\frac{1}{2}}^{trial} - \frac{1}{2} \frac{\bar{\gamma}_{n+\frac{1}{2}}}{1 + \bar{\mu}_n} \mathbf{N}_{n+\frac{1}{2}}^{trial} \end{aligned} \quad (45)$$

With these results in hand, the consistent elasto-damage tangent modulus,  $\mathbf{C}_{n+\frac{1}{2}}^{ed} = \frac{\partial \boldsymbol{\sigma}_{n+\frac{1}{2}}}{\partial \bar{\boldsymbol{\epsilon}}_{n+\frac{1}{2}}}$ , can be

easily obtained as

$$\begin{aligned} \mathbf{C}_{n+\frac{1}{2}}^{ed} &= \frac{\mathbf{C}^e}{1 + \bar{\mu}_n} \left( 1 - \frac{\bar{\gamma}_{n+\frac{1}{2}}}{2(1 + \bar{\mu}_n) \|\boldsymbol{\sigma}_{n+\frac{1}{2}}^{trial}\|_{\mathbf{D}^e}} \right) \\ &+ \frac{1}{2(1 + \bar{\mu}_n)^2} \left( \frac{\bar{\gamma}_{n+\frac{1}{2}}}{\|\boldsymbol{\sigma}_{n+\frac{1}{2}}^{trial}\|_{\mathbf{D}^e}} - \frac{1}{\frac{\bar{\eta}}{\Delta t} + \frac{1}{2(1+\bar{\mu}_n)} + \frac{\bar{K}}{2E}} \right) \mathbf{N}_{n+\frac{1}{2}}^{trial} \otimes \mathbf{N}_{n+\frac{1}{2}}^{trial} \end{aligned} \quad (46)$$

Once passed the peak resistance, we start the local computation of the softening phase by considering the elastic trial state, according to

$$\bar{\gamma}_{n+\frac{1}{2}} = 0, \bar{\xi}_{n+\frac{1}{2}}^{trial} = \bar{\xi}_n, \bar{\mathbf{Q}}_{n+\frac{1}{2}}^{trial} = \bar{\mathbf{Q}}_n, \bar{q}_{n+\frac{1}{2}}^{trial} = \bar{q}_n \text{ and } \mathbf{t}_{\Gamma_s, n+\frac{1}{2}}^{trial} = \bar{\mathbf{Q}}_n^{-1} \bar{\mathbf{u}}_{n+\frac{1}{2}}^{(i)}, i = 1, 2 \quad (47)$$

If both damage functions take negative or zero values, the trial step solution can be accepted as final and no evolution of the internal variables is needed.

$$\begin{cases} \bar{\Phi}_{1, n+\frac{1}{2}}^{trial} = \mathbf{n} \cdot \mathbf{t}_{\Gamma_s, n+\frac{1}{2}}^{trial} - \left( \bar{\sigma}_f - \bar{q}_{n+\frac{1}{2}}^{trial} \right) \leq 0 \\ \bar{\Phi}_{2, n+\frac{1}{2}}^{trial} = \left| \mathbf{m} \cdot \mathbf{t}_{\Gamma_s, n+\frac{1}{2}}^{trial} \right| - \left( \bar{\sigma}_s - \frac{\bar{\sigma}_s}{\bar{\sigma}_f} \bar{q}_{n+\frac{1}{2}}^{trial} \right) \leq 0 \end{cases} \quad (48)$$

In contrast, if any of yield functions takes positive values, computing the value of the corresponding Lagrange multiplier  $\bar{\gamma}_{i, n+\frac{1}{2}}$  ( $i = 1, 2$ ) and updating the final values of the internal variables are compulsory, namely

$$\begin{aligned} \bar{\mathbf{Q}}_{n+1} &= \bar{\mathbf{Q}}_n + \bar{\gamma}_{1, n+\frac{1}{2}} \frac{1}{\mathbf{n} \cdot \mathbf{t}_{\Gamma_s, n+\frac{1}{2}}} \mathbf{n} \otimes \mathbf{n} + \bar{\gamma}_{2, n+\frac{1}{2}} \frac{1}{\left| \mathbf{m} \cdot \mathbf{t}_{\Gamma_s, n+\frac{1}{2}} \right|} \mathbf{m} \otimes \mathbf{m} \\ \bar{\mathbf{Q}}_{n+\frac{1}{2}} &= \frac{\bar{\mathbf{Q}}_{n+1} + \bar{\mathbf{Q}}_n}{2} \\ \bar{\xi}_{n+1} &= \bar{\xi}_n + \bar{\gamma}_{1, n+\frac{1}{2}} + \bar{\gamma}_{2, n+\frac{1}{2}} \frac{\bar{\sigma}_s}{\bar{\sigma}_f} \\ \bar{\xi}_{n+\frac{1}{2}} &= \frac{\bar{\xi}_{n+1} + \bar{\xi}_n}{2} \end{aligned} \quad (49)$$

resulting in two possibilities to express the total deformation in terms of stress

$$\bar{\mathbf{u}}_{n+\frac{1}{2}}^{(i)} = \begin{cases} \bar{\mathbf{Q}}_n \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}^{trial} \\ \bar{\mathbf{Q}}_{n+\frac{1}{2}} \mathbf{t}_{\Gamma, s, n+\frac{1}{2}} \end{cases} \quad (50)$$

We can establish the relationship between the final and the trial value of driving traction acting on the crack by combining Eqs. (49) and (50)

$$\mathbf{t}_{\Gamma, s, n+\frac{1}{2}} = \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}^{trial} - \bar{\mathbf{Q}}_n^{-1} \left[ \bar{\gamma}_{1, n+\frac{1}{2}} \mathbf{n} + \bar{\gamma}_{2, n+\frac{1}{2}} \text{sign} \left( \mathbf{m} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}^{trial} \right) \mathbf{m} \right] \quad (51)$$

$$\Rightarrow \begin{cases} \mathbf{n} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}} = \mathbf{n} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}^{trial} - \bar{\gamma}_{1, n+\frac{1}{2}} \bar{\mathbf{Q}}_{nn, n}^{-1} \\ \left| \mathbf{m} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}} \right| = \left| \mathbf{m} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}^{trial} \right| - \bar{\gamma}_{2, n+\frac{1}{2}} \bar{\mathbf{Q}}_{mm, n}^{-1} \\ \text{sign} \left( \mathbf{m} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}} \right) = \text{sign} \left( \mathbf{m} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}^{trial} \right) \end{cases} \quad (52)$$

The expression of the final value of the damage function in terms of its trial values can be written as

$$\begin{cases} \bar{\Phi}_1 \left( \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}, \bar{q}_{n+\frac{1}{2}} \right) = \bar{\Phi}_{1, n+\frac{1}{2}}^{trial} - \bar{\gamma}_{1, n+\frac{1}{2}} (\mathbf{n} \cdot \bar{\mathbf{Q}}_n \mathbf{n}) - (\bar{q}_{n+\frac{1}{2}} - \bar{q}_n) \\ \bar{\Phi}_2 \left( \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}, \bar{q}_{n+\frac{1}{2}} \right) = \bar{\Phi}_{2, n+\frac{1}{2}}^{trial} - \bar{\gamma}_{2, n+\frac{1}{2}} (\mathbf{m} \cdot \bar{\mathbf{Q}}_n \mathbf{m}) \text{sign} \left( \mathbf{m} \cdot \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}^{trial} \right) - \frac{\bar{\sigma}_s}{\bar{\sigma}_f} (\bar{q}_{n+\frac{1}{2}} - \bar{q}_n) \end{cases} \quad (53)$$

For a multi-surface damage model of this kind, we must take into account the total following different possibilities concerning loading-unloading conditions in computational procedure, namely:

Table 1 Different cases for numerical integration of the softening part

	$\bar{\gamma}_{1, n+\frac{1}{2}} < 0$	$\bar{\gamma}_{1, n+\frac{1}{2}} > 0$
$\bar{\gamma}_{2, n+\frac{1}{2}} < 0$	Elastic step	Damage step in mode I
$\bar{\gamma}_{2, n+\frac{1}{2}} > 0$	Damage step in mode II	Damage step where both mode I and mode II are active simultaneously

Finally, we compute the elasto-damage tangent modulus for the next step, according to

$$\bar{\mathbf{C}}_{n+\frac{1}{2}}^{ed} = \frac{\partial \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}}{\partial \bar{\mathbf{u}}_{n+\frac{1}{2}}} = \begin{cases} \bar{\mathbf{Q}}_n^{-1} - \sum_{i, j=1}^2 \left[ \mathbf{G}_{ij, n+\frac{1}{2}} \right]^{-1} \left( \bar{\mathbf{Q}}_n^{-1} \frac{\partial \bar{\Phi}_i}{\partial \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}} \right) \otimes \left( \bar{\mathbf{Q}}_n^{-1} \frac{\partial \bar{\Phi}_i}{\partial \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}} \right) \\ \bar{\mathbf{Q}}_n^{-1} - \frac{1}{\frac{\partial \bar{\Phi}_i}{\partial \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}} \cdot \bar{\mathbf{Q}}_n^{-1} \frac{\partial \bar{\Phi}_i}{\partial \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}}} \left( \bar{\mathbf{Q}}_n^{-1} \frac{\partial \bar{\Phi}_i}{\partial \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}} \right) \otimes \left( \bar{\mathbf{Q}}_n^{-1} \frac{\partial \bar{\Phi}_i}{\partial \mathbf{t}_{\Gamma, s, n+\frac{1}{2}}} \right) \end{cases} \quad (54)$$

Having computed the internal variables in the local phase of the operator split solution procedure, we proceed to the global phase to check the equilibrium. In this phase, the mid-point scheme and the following residual equations established by applying incompatible mode method (see Simo and Rifai 1990 or Ibrahimbegovic and Wilson 1991) at the time step  $t_{n+\frac{1}{2}}$  and iteration  $i$  are used for computations

$$\begin{cases} \mathbf{r}_{n+\frac{1}{2}}^{(e),(i)} = \mathbb{A}_{e=1}^{nel} \left[ \mathbf{f}_{ext,n+\frac{1}{2}}^{(e),(i)} - \mathbf{f}_{int,n+\frac{1}{2}}^{(e),(i)}(d_{n+\frac{1}{2}}) \right] - \mathbf{M}\mathbf{a}_{n+\frac{1}{2}}^{(e),(i)} & \text{for } \mathbf{x} \in \Omega \setminus \Gamma_s \\ \mathbf{h}_{n+\frac{1}{2}}^{(e),(i)} = \int_{\Omega^e} \bar{\mathbf{G}}_v^T \boldsymbol{\sigma}_{n+\frac{1}{2}}^{(e),(i)} d\Omega^e + \int_{\Gamma_s} \bar{\bar{\mathbf{G}}}_v^T \mathbf{t}_{s,n+\frac{1}{2}} d\Gamma_s = 0 & \text{for } \mathbf{x} \in \Gamma_s \end{cases} \quad (55)$$

$$\begin{aligned} \mathbf{d}_{n+\frac{1}{2}} &= \frac{\mathbf{d}_n + \mathbf{d}_{n+1}}{2} \\ \mathbf{v}_{n+\frac{1}{2}} &= \frac{\mathbf{d}_{n+1} - \mathbf{d}_n}{\Delta t} = \frac{2}{\Delta t} (\mathbf{d}_{n+\frac{1}{2}} - \mathbf{d}_n) \\ \mathbf{a}_{n+\frac{1}{2}} &= \frac{\mathbf{v}_{n+1} - \mathbf{v}_n}{\Delta t} = -\frac{2}{\Delta t} \mathbf{v}_n + \frac{4}{\Delta t^2} (\mathbf{d}_{n+\frac{1}{2}} - \mathbf{d}_n) \end{aligned} \quad (56)$$

where  $\mathbf{M}$ ,  $\mathbf{f}_{ext,n+\frac{1}{2}}^{(e),(i)}$  and  $\mathbf{f}_{int,n+\frac{1}{2}}^{(e),(i)}(d_{n+\frac{1}{2}})$  are the element mass matrix, external and internal forces, respectively

$$\begin{aligned} \mathbf{M} &= \int_{\Omega^e} \rho \mathbf{N}^T \mathbf{N} d\Omega^e \\ \mathbf{f}_{ext,n+\frac{1}{2}}^{(e),(i)} &= \int_{\Omega^e} \mathbf{N} \mathbf{b}_{n+\frac{1}{2}} \mathbf{N}^T d\Omega^e + \left[ \mathbf{N}^T \bar{\mathbf{t}}_{n+\frac{1}{2}} \right]_{\Gamma_\sigma} \\ \mathbf{f}_{int,n+\frac{1}{2}}^{(e),(i)} &= \int_{\Omega^e} \mathbf{B}^T \boldsymbol{\sigma}_{n+\frac{1}{2}}^{(e),(i)} d\Omega^e \end{aligned} \quad (57)$$

The linearized form of the system of equilibrium equations in (55) can then be obtained by using Newton-Raphson method together with interpolations described in the previous section, according to

$$\begin{bmatrix} \mathbb{A}_{e=1}^{nel} \hat{\mathbf{K}}^{(e)} & \mathbb{A}_{e=1}^{nel} \mathbf{F}^{(e)} \\ \mathbf{F}^{T,(e)} & \mathbf{H}^{(e)} \end{bmatrix}_{n+\frac{1}{2}}^i \begin{pmatrix} \Delta \mathbf{d}_{n+\frac{1}{2}}^{(e),(i)} \\ \Delta \bar{\bar{\mathbf{u}}}_{n+\frac{1}{2}}^{(e),(i)} \end{pmatrix} = \begin{pmatrix} \mathbb{A}_{e=1}^{nel} \mathbf{r}_{n+\frac{1}{2}}^{(e),(i)} \\ \mathbf{h}_{n+\frac{1}{2}}^{(e),(i)} \end{pmatrix} \quad (58)$$

in which the parts of element stiffness matrix are as follows

$$\begin{aligned}
\widehat{\mathbf{K}}_{n+\frac{1}{2}}^{(e),(i)} &= \mathbf{K}_{n+\frac{1}{2}}^{(e),(i)} + \frac{4}{\Delta t^2} \mathbf{M} \\
\mathbf{K}_{n+\frac{1}{2}}^{(e),(i)} &= \frac{\partial \mathbf{f}_{int,n+\frac{1}{2}}^{(e),(i)}}{\partial \mathbf{d}} = \int_{\Omega^e} \mathbf{B}^T \mathbf{C}_{n+\frac{1}{2}}^{ed} \mathbf{B} d\Omega^e \\
\mathbf{F}_{n+\frac{1}{2}}^{(e),(i)} &= \frac{\partial \mathbf{f}_{int,n+\frac{1}{2}}^{(e),(i)}}{\partial \bar{\mathbf{u}}} = \int_{\Omega^e} \mathbf{B}^T \mathbf{C}_{n+\frac{1}{2}}^{ed} \bar{\mathbf{G}}_r d\Omega^e \\
\mathbf{F}_{n+\frac{1}{2}}^{T,(e),(i)} &= \frac{\partial \mathbf{h}_{n+\frac{1}{2}}^{(e),(i)}}{\partial \mathbf{d}} = \int_{\Omega^e} \bar{\mathbf{G}}_v^T \mathbf{C}_{n+\frac{1}{2}}^{ed} \mathbf{B} d\Omega^e + \int_{\Gamma_s} \bar{\mathbf{G}}_v^T \frac{\partial \mathbf{t}_{\Gamma_s}}{\partial \mathbf{d}} d\Gamma_s = \int_{\Omega^e} \bar{\mathbf{G}}_v^T \mathbf{C}_{n+\frac{1}{2}}^{ed} \mathbf{B} d\Omega^e \\
\mathbf{H}_{n+\frac{1}{2}}^{(e),(i)} &= \frac{\partial \mathbf{h}_{n+\frac{1}{2}}^{(e),(i)}}{\partial \bar{\mathbf{u}}} = \int_{\Omega^e} \bar{\mathbf{G}}_v^T \mathbf{C}_{n+\frac{1}{2}}^{ed} \bar{\mathbf{G}}_r d\Omega^e + \int_{\Gamma_s} \bar{\mathbf{G}}_v^T \underbrace{\frac{\partial \mathbf{t}_{\Gamma_s}}{\partial \bar{\mathbf{u}}}}_{\bar{\mathbf{C}}_{n+\frac{1}{2}}^{ed}} d\Gamma_s
\end{aligned} \tag{59}$$

Since the second equation is condensed at the element level the system (58) is reduced to the classical form

$$\mathbb{A}_{e=1}^{nel} \left( \mathbf{K}_{eff,n+\frac{1}{2}}^{(e),(i)} \Delta \mathbf{d}_{n+\frac{1}{2}}^{(e),(i)} \right) = \mathbb{A}_{e=1}^{nel} \mathbf{r}_{eff,n+\frac{1}{2}}^{(e),(i)} \tag{60}$$

where  $\mathbf{K}_{eff,n+\frac{1}{2}}^{(e),(i)}$ ,  $\mathbf{r}_{eff,n+\frac{1}{2}}^{(e),(i)}$ , that respectively stand for the effective stiffness matrix and effective residual of element, are defined by

$$\begin{aligned}
\mathbf{K}_{eff,n+\frac{1}{2}}^{(e),(i)} &= \widehat{\mathbf{K}}_{n+\frac{1}{2}}^{(e),(i)} - \mathbf{F}_{n+\frac{1}{2}}^{T,(e),(i)} \left( \mathbf{H}_{n+\frac{1}{2}}^{(e),(i)} \right)^{-1} \mathbf{F}_{n+\frac{1}{2}}^{(e),(i)} \\
\mathbf{r}_{eff,n+\frac{1}{2}}^{(e),(i)} &= \mathbf{r}_{n+\frac{1}{2}}^{(e),(i)} - \underbrace{\mathbf{F}_{n+\frac{1}{2}}^{(e),(i)} \left( \mathbf{H}_{n+\frac{1}{2}}^{(e),(i)} \right)^{-1} \mathbf{h}_{n+\frac{1}{2}}^{(e),(i)}}_{=0}
\end{aligned} \tag{61}$$

#### 4. Numerical simulations

We present in this section several numerical simulations that illustrate and evaluate the performance of the model. Moreover, in order to validate the capability of the mid-point scheme these obtained numerical results are then compared with the ones computed with Newmark scheme. In all examples: (i) the plane strain hypothesis is imposed; (ii) the time-dependency of the application of loads is linear increase in time; (iii) only type of fine mesh is employed for computation. GMSH software (Geuzaine and Remacle 2009) is used to generate meshes with constant strain triangle (CST) elements. The implementation of the proposed model and all the computations are carried out with an enhanced version of the computer program FEAP, developed

by R.L. Taylor at UC Berkeley (e.g., see Zienkiewicz and Taylor (1989) for the description of a PC version).

#### 4.1 Simple tension test

In this first example, a rectangular strip of 200 mm × 100 mm × 1 mm subjected to homogenous displacement-controlled tension applied at the right free-end is considered, see Fig. 3(a) for an illustration. It is important to note that a single element in mesh (red area) is slightly weakened to better orientate the macro-crack occurrence. Table 2 indicates the chosen values of material parameters of the specimen.

Table 2 Material properties of the specimen

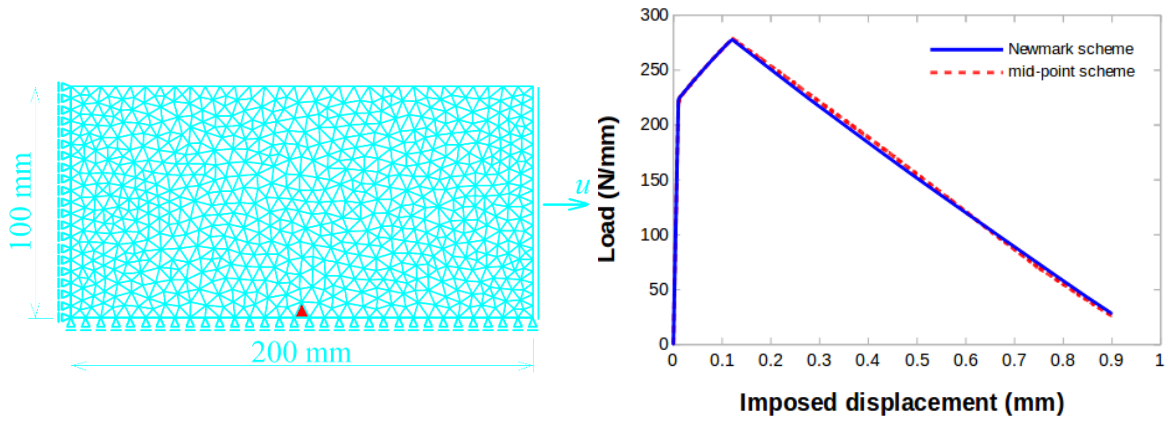
<i>Continuous model</i>	
Young modulus	38 GPa
Poisson's coefficient	0.18
Density mass	2600 kg/m <sup>3</sup>
$\bar{\sigma}_f$	2 Mpa
$\bar{K}$	1,000 MPa
<i>Discrete model</i>	
$\bar{\sigma}_f$	2.55 MPa
$\bar{\sigma}_s/\bar{\sigma}_f$	2.35 MPa (weakened element)
$\bar{\beta}$	0.3
	25.5 MPa/mm

According to the results in Figs. 3(c) and (d), it can be seen that for both schemes macro-cracks originate from the weakened element in mesh and then go through the center of neighboring elements in the direction perpendicular to the principal stress after the maximum principal stress reaches the chosen damage threshold value. In addition, a comparison between the results obtained with the mid-point scheme and the Newmark scheme in terms of the load versus displacement response (Fig. 3(b)) and in terms of crack opening at the end of the computation (Figs. 3(e) and (f)) also shows a small difference.

#### 4.2 Three-point bending test

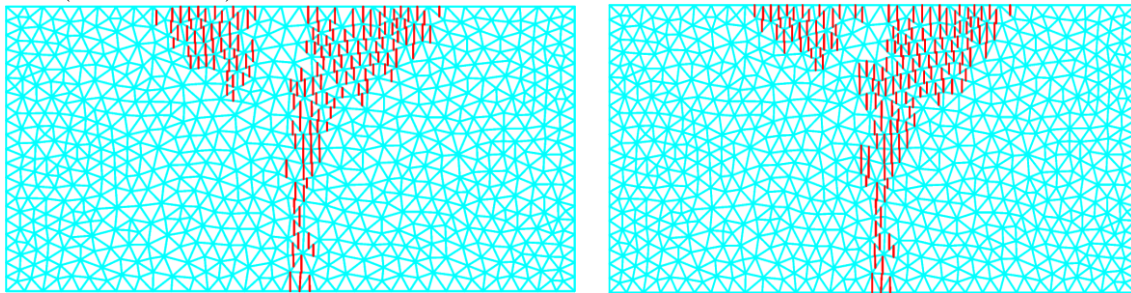
The second example presents the classical three-point bending test on a notched concrete beam (see Petersson (1981), Rots *et al.* (1985) and references therein). Fig. 4 describes the geometry of the specimen (a 1800 mm × 500 mm × 1mm plain concrete beam with a 20 mm × 200 mm × 1mm notch at its bottom center), the boundary conditions and the corresponding finite element mesh (1722 elements). In order to ensure this element test is performed under displacement control, the beam is simply loaded by imposed downward displacements at its center top. The set of considered material parameters is given in Table 3.





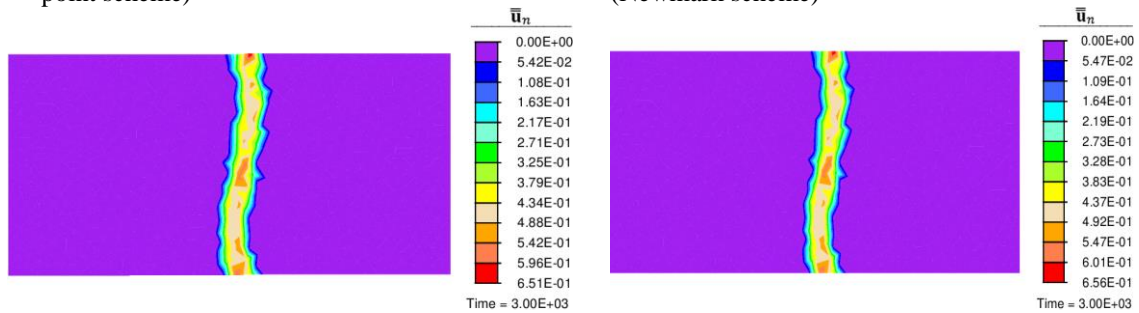
(a) Geometry, boundary conditions and finite element mesh (1402 elements)

(b) Load versus displacement diagram



(c) Cracks at the end of simulation time (mid-point scheme)

(d) Cracks at the end of simulation time (Newmark scheme)



(e) Crack opening [mm] at the end of simulation time (mid-point scheme)

(f) Crack opening [mm] at the end of simulation time (Newmark scheme)

Fig. 3 Set up for the simple tension test (a), and comparison between the mid-point scheme and the Newmark scheme (b), (c), (d), (e), (f)

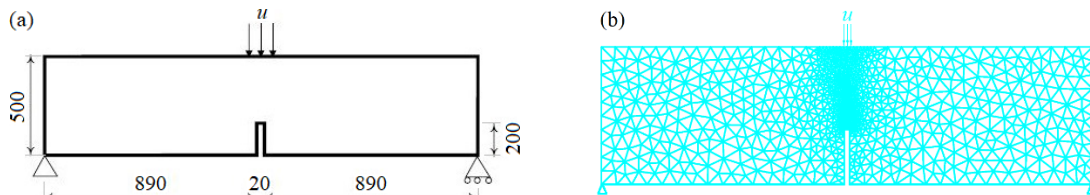


Fig. 4 Three-point bending test: problem definition (a) Geometrical properties (in mm) and boundary conditions, (b) Finite element mesh (1722 elements)

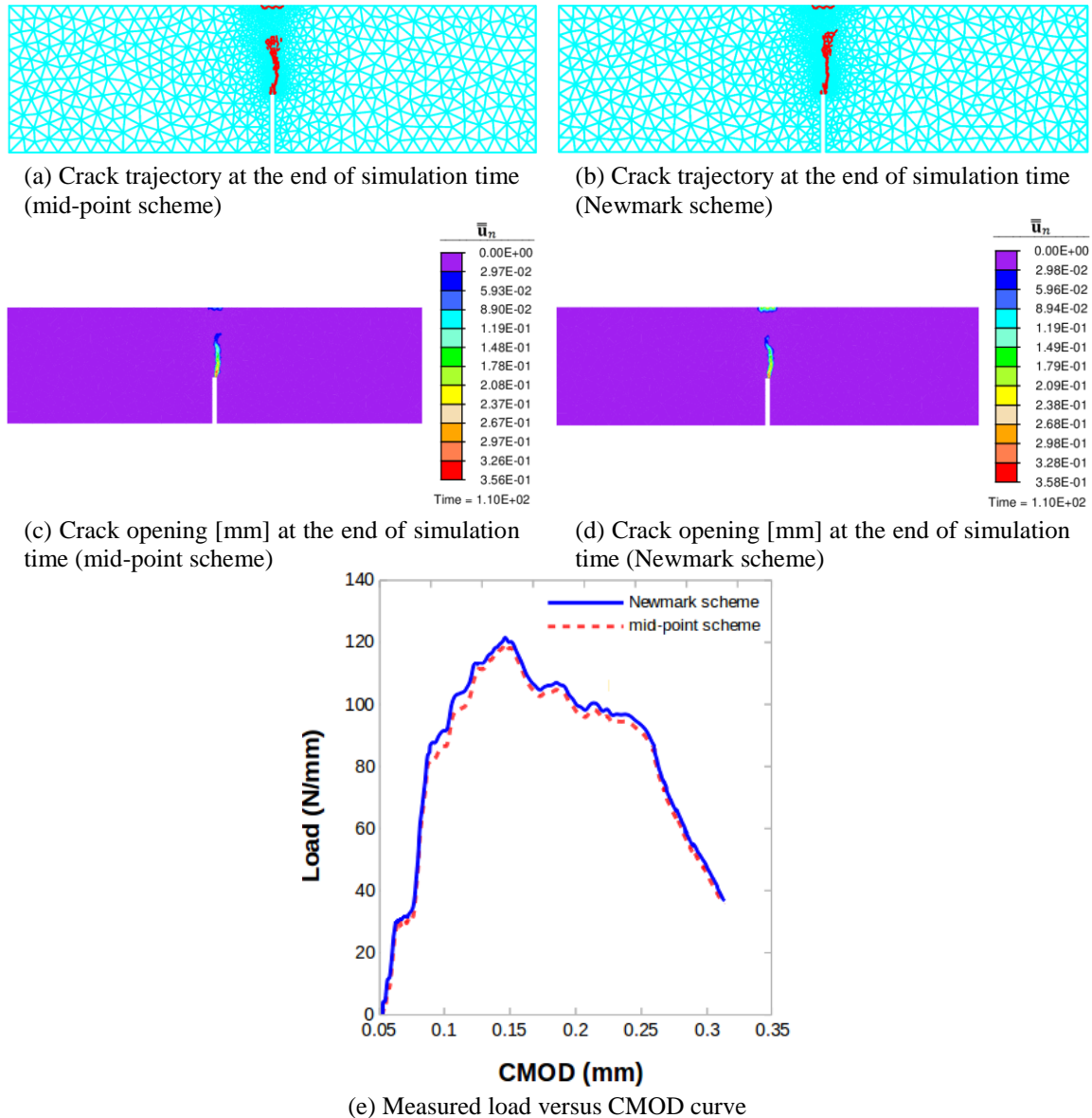


Fig. 5 Comparison between the mid-point scheme and the Newmark scheme for the three-point bending test

Results in Figs. 5(a) and (b) point out that the trajectory of development of the crack for the mid-point scheme and the Newmark scheme is fairly the same and agrees quite well with experimental results. Namely, from the experimental point of view, the crack is allowed to initiate at the notch and propagates perpendicularly to the length of the beam. Moreover, it can be observed from Figs. 5(c) and (d) that the values of crack opening computed with the mid-point scheme and the Newmark scheme are almost equivalent.

As for Fig. 5(e) in which measured load is plotted against the crack mouth opening displacement (CMOD), we find once again that the global response for both schemes above is very

Table 3 Material properties of the model in the three-point bending test

<i>Continuous model</i>	
Young modulus	38 GPa
Poisson's coefficient	0.1
Density mass	2600 kg/m <sup>3</sup>
$\bar{\sigma}_f$	2.2 Mpa
$\bar{K}$	1,000 MPa
<i>Discrete model</i>	
$\bar{\bar{\sigma}}_f$	2.35 MPa
$\bar{\bar{\beta}}$	23.5 MPa/mm
$\bar{\bar{\sigma}}_s$	0.235 MPa

close and shows a general rule with absolute vertical or relative horizontal evolution of displacement as a function of applied loading.

Finally, it is interesting to note that for the mid-point scheme by adding viscosity parameter and by employing the time step  $\Delta t = 2 \cdot 10^{-2} s$  which is twice as big as the time step exploited for the Newmark scheme ( $\Delta t = 10^{-2} s$ ) the total number of iteration is significantly reduced (23,841 versus 25,125 by the Newmark scheme) while the convergence of the solution is still ensured (in case of the Newmark scheme the solution cannot produce a good convergence with an increase to  $2 \cdot 10^{-2} s$  of  $\Delta t$ ).

#### 4.3 Four-point bending test

We deal now with the challenging benchmark problem of a notched concrete beam under four-point bending, reported by Arrea and Ingrassia (1982) among others. The geometry of the problem is sketched in Fig. 6(a), where four blocks located between the imposed load and the concrete beam as well as between the supports and the concrete beam are steel caps with Young's modulus  $E = 288 \text{ GPa}$ , density mass of  $7830 \text{ kg/m}^3$  and Poisson's coefficient equal to 0.18. The finite element mesh (1710 CST elements) is presented in Fig. 6(b). The main difference with the three-point bending test considered in Section 4.1 is that in this case the external load is applied on the steel caps at the top surface of the beam. The material properties are given in Table 4.

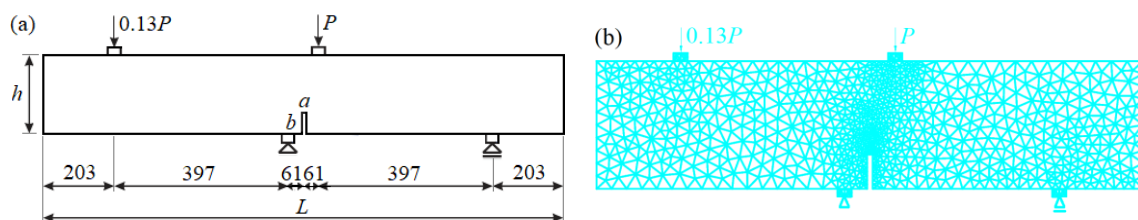
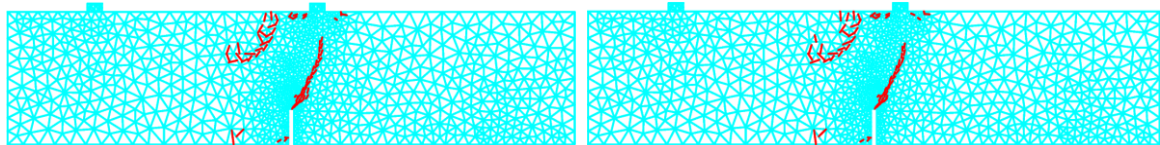


Fig. 6 Notched concrete specimen: (a) geometry (in mm) with  $L = 1322 \text{ mm}$ ,  $h = 306 \text{ mm}$ ,  $a = 14 \text{ mm}$ ,  $b = 82 \text{ mm}$  and boundary conditions, (b) finite element mesh (1710 elements)

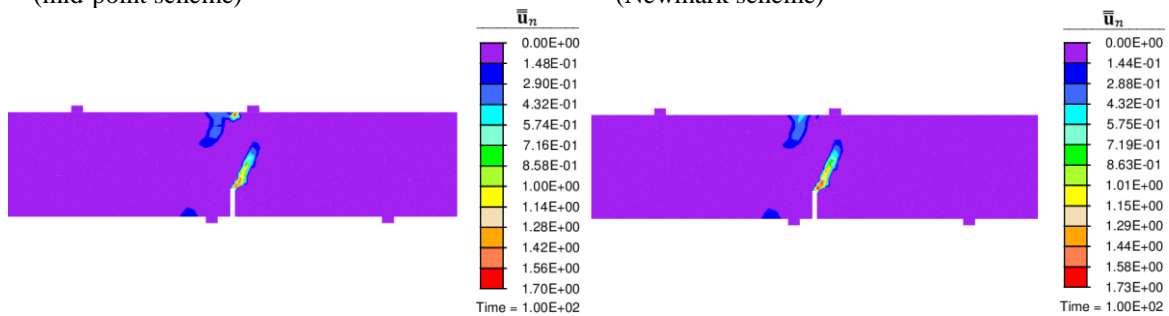
Table 4 Material properties for the four-point bending test

<i>Continuous model</i>	
Young modulus	28.8 GPa
Poisson's coefficient	0.18
Density mass	2600 kg/m <sup>3</sup>
$\bar{\sigma}_f$	2.6 MPa
$\bar{K}$	1,000 MPa
<i>Discrete model</i>	
$\bar{\sigma}_f$	2.8 MPa
$\bar{\beta}$	28 MPa/mm
$\bar{\sigma}_s$	0.28 MPa



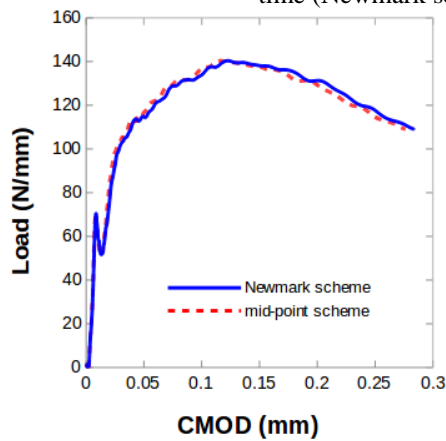
(a) Crack trajectory at the end of simulation time (mid-point scheme)

(b) Crack trajectory at the end of simulation time (Newmark scheme)



(c) Crack opening [mm] at the end of simulation time (mid-point scheme)

(d) Crack opening [mm] at the end of simulation time (Newmark scheme)



(e) Load-CMOD response

Fig. 7 Comparison between the mid-point scheme and the Newmark scheme for the four-point bending test

As can be seen from results in Figs. 7(a) and (b), the main crack in both schemes, the mid-point and Newmark, starts at the top right corner of the notch and then propagates up and to the right, the same as observed in experiment. However, different from static/quasi-static case, in the framework of dynamic loading, beside this main crack, secondary crack propagated at the position close to the external load  $P$  of the specimen since no tracking algorithm has been used to enforce only one crack. It is worth noting that the cracks are propagated by the stress concentration at the crack tip, while the failure direction is governed by the stress distribution.

Turning to the Figs. 7(c) and (d), where the main crack and the secondary crack predicted above are revealed more obviously, we can figure out that the local results in terms of crack opening remain quite similar for these two types of scheme.

Last but not least, in order to seek a good agreement between the mid-point scheme and the Newmark scheme a comparison in terms of global response is needed. More specifically, Fig. 7(e), which plots the load versus CMOD (crack mouth opening displacement) curve, shows a small gap and a quite identical trend in the path of computation of these two schemes, namely: the evolution of displacement as a function of applied loading.

## 5. Conclusions

In this paper, a two-dimensional continuum viscodamage-embedded discontinuity model, which combines the pre-peak nonlinear and rate-sensitive hardening response of the material behavior, representing the fracture-process zone creation and the post-peak response, involving the macro-crack creation accompanied by exponential softening, has been developed. The element tests and representative numerical simulations presented above illustrate good performance of the proposed model. Specially, by adding the viscosity parameter and by using the second-order mid-point scheme that allows bigger time steps the time for computation can be significantly reduced while the convergence is still ensured well. This feature is the main advantage of the presented scheme in comparison with the Newmark scheme and is the main novelty of this work. As a consequence, the proposed model is very suitable for long computations and high frequency problems.

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